

ON THE MECHANISM OF AEROACOUSTIC INITIATION OF PULSED QUASI-DETONATION COMBUSTION IN AN AIR-BREATHING EJECTOR PULSEJET*

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Abstract: The present paper discusses the design of a pulse-jet engine in which a new mechanism of deflagration-to-detonation transition and establishment of a mode close to the detonation combustion or quasi-detonation mode is realized. It is found that the possibility of such a transition is provided by a special design of the gas duct which has a double bend leading to the formation of a specific vortex structure of the internal flow allowing the acoustic tuning of the gas duct to reach such combustion modes.

Keywords: valveless ejector pulse-jet engine; double gas-jet bend; acoustic tuning; quasi-detonation; spherical detonation

DOI: 10.30826/CE22150309

EDN: KIEWCR

Figure Captions

Figure 1 Calculated flow structure inside the gas duct of an ejector pulse-jet engine: (a) longitudinal section; and (b) cross section of the combustion chamber (section A–A)

Figure 2 Schematic diagram of the internal flow in the combustion chamber and resonator tube explaining the process of vortex development, appearance of precession, and destruction of vortices

Figure 3 Snapshots of the temperature fields in the engine gas duct during one pulsation cycle at a frequency of 100 Hz and approaching flow velocity of 500 m/s: (a) beginning of a new pulsation cycle, the nucleation of the separation zone under the canopy; (b) start of combustion in the separation zone under the canopy; (c) evolution of combustion in the separation zone under the canopy; (d) start of gas throwing by longitudinal vortices into the separation zone under the canopy, deformation of the separation zone is visible; (e) evolution of the throwing process in the separation zone; and (f) end of the pulsation cycle

Figure 4 Typical spectrum of pressure pulsations at the nozzle section of acoustically tuned gas duct ($L = 1410$ mm) at different frequencies of longitudinal oscillations: 1 — 100 Hz; 2 — 110; and 3 — 120 Hz

Figure 5 Layout of the “flat” engine and a prototype installation for aeroacoustic tests, 1, 2, and 3 — separation zones. Dimensions are in millimeters

Figure 6 Calculated flow structure inside the gas duct of the “flat” engine

Figure 7 Spectra of acoustic oscillations at an excitation frequency of 120 Hz and different length of the resonator tube: 1 — 1300 mm; 2 — 1360; 3 — 1380; 4 — 1400; and 5 — 1420 mm. Blowing velocity is 60 m/s, “flat” gas duct

Figure 8 Schematic layout of the gas duct with a cylindrical combustion chamber. Dimensions are in millimeters

Figure 9 Internal flow in the gas duct at a blowing velocity of 60 m/s

Figure 10 Variation of the circumferential vortex velocity W_r depending on the blowing velocity W for different engine gas duct designs: 1 — design of Fig. 1; and 2 — design of Fig. 6

Figure 11 Spectrograms of acoustic pressure pulsations (frequency 120 Hz): 1 — 1350 mm without blowing; 2 — 1350 mm, $W = 60$; 3 — 1370 mm; 4 — 1385; 5 — 1400; and 6 — 1430 mm

Figure 12 Schematic of the experimental installation. Dimensions are in millimeters

Figure 13 Spectrograms taken at the 1380-millimeter gas duct, 60 m/s: (a) 90 Hz; (b) 100; and (c) 110 Hz; 1 — combustion chamber; and 2 — nozzle cross section

*This paper is based on the work that was presented at the 13th International Colloquium on Pulsed and Continuous Detonations (ICPCD), April 18–21, 2022, St. Petersburg, Russia.

Figure 14 Spectrograms taken at the 1410-millimeter gas duct, 60 m/s: (a) 90 Hz; (b) 100; and (c) 110 Hz; 1 — combustion chamber; and 2 — nozzle cross section

Figure 15 Schematic illustration of the flow in the combustion chamber

Figure 16 Idealized pulsed combustion cycle represented as pressure changes in the combustion chamber

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Received August 20, 2021

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